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## Description

### Background of the Invention

5 This invention relates to treated alumina.

Supported chromium oxide catalysts have long been used to prepare olefin polymers in hydrocarbon solution or slurry to give products having excellent characteristics from many standpoints. A number of supports have long been broadly disclosed in the art for chromium oxide catalysts including silica, alumina, thoria, zirconia, silica alumina, and other refractory materials. However, as a practical matter only predomi-  
 10 nately silica supports have achieved substantial commercial success. Alumina which is almost always included in the prior art in the list of suitable supports, while operable, invariably causes productivity to be extremely low. The preferred prior art support, silica, also suffers from disadvantages among which is the inability to produce ultra high molecular weight polymer using hexavalent chromium.

### 15 Summary of the Invention

It is an object of this invention to provide an improved alumina.

It is a further object of this invention to provide a chromium catalyst capable of giving high productivity.

It is a further object of this invention to provide a chromium catalyst capable of producing ultra high  
 20 molecular weight polymer.

It is a further object of this invention to provide a catalyst suitable for use in slurry polymerization systems.

It is still a further object of this invention to produce a catalyst capable of making branched polyethylene in the 0.960-0.930 density range from ethylene alone.

25 It is still a further object of this invention to provide catalysts having a wide sensitivity to H<sub>2</sub> as a MW regulating agent, from almost no sensitivity to highly sensitive.

It is still a further object of this invention to prepare intimate bimodal mixtures of high and low MW polymers for use in film and blow molding.

30 It is still yet a further object of this invention to overcome the difficulties traditionally associated with both alumina and silica as supports for chromium-catalyzed olefin polymerization.

In accordance with one aspect of this invention a silicated alumina is provided, which alumina can also be fluorided and/or phosphated.

In accordance with another aspect of this invention, a fluorided and/or silicated alumina support is used for a chromium olefin polymerization catalyst.

35 In accordance with still another aspect of the invention aluminum phosphate is formed in the pores of alumina.

### Brief Description of the Drawings

40 FIGURE 1 shows the relationship between density and melt viscosity for UHMWPE polymers made with a variety of catalyst systems.

FIGURE 2 shows the relationship between polymer density and intrinsic viscosity.

### Description of the Preferred Embodiments

45 The alumina selected for surface treatment according to this invention can also contain minor amounts of other ingredients which do not adversely affect the quality of the final catalyst but it is generally essentially pure alumina. The alumina can be made as is well known in the art, for instance, by reacting sodium aluminate, which is basic, with aluminum sulfate, which is acidic, or by neutralizing an aluminum salt  
 50 with a base such as ammonia or ammonia hydroxide, or by flame hydrolysis. If desired, the alumina can be calcined prior to treatment for instance by heating in air at a temperature of 300-900 °C, preferably 500-800 °C but this is not essential.

The amount of combined fluorine is generally in the range of 0.1 to 5, preferably 0.5 to 3 weight percent fluorine, based on the weight of the alumina.

55 The surface silicated alumina is prepared by contacting the alumina with a silicating agent, generally by forming a slurry of the alumina in a solution of a silicating agent. Generally a lower alcohol such as a one to 6 carbon atom alcohol is used as the solvent. After the solution and alumina are mixed the composite is dried. Alternatively the alumina can be subjected to a vapor of the silicating agent. The silicating agent is

used in an amount to give 0.2 to 20, preferably 0.5 to 10 weight percent silica, based on the weight of the alumina. The resulting product is alumina with a surface coating of silica which is different than conventional silica-alumina.

The resulting novel product is suitable as a catalyst support but is also suitable for use broadly where alumina is utilized.

The term "silicating agent" is meant to encompass silicon alkoxides and aryloxides and their hydrolysis products, e.g. alkoxysiloxanes, which upon calcining in the activation of the support or catalyst yield high purity, refractory silica. Examples of such compounds include tetramethoxysilane, tetraethoxysilane (tetraethyl orthosilicate), tetra(2-ethylbutoxy)silane, tetrakis(2-methoxyethoxy)silane, tetraphenoxysilane, and phenyltriethoxysilane and their hydrolysis products and mixtures thereof. A presently preferred silicating agent comprises a polymeric siloxane form of tetraethoxysilane containing the equivalent of 40 weight per cent silica. Such a composition is commercially sold as Silbond® 40 by Stauffer Chemical Co., Westport, Connecticut.

The silicating agent can be converted to surface silica after the treatment by calcining as described above or the treated alumina can be allowed to stand until hydrolysis converts the treating agent to silica.

In accordance with another embodiment the alumina is treated with a fluoriding agent so as to incorporate fluorine onto the alumina to produce a support for a hexavalent chromium catalyst which is used with a cocatalyst or as a support for an organochromium catalyst. A preferred fluoriding agent is ammonium bifluoride,  $\text{NH}_4\text{HF}_2$ . Also suitable is ammonium silicofluoride,  $(\text{NH}_4)_2\text{SiF}_6$ . While ammonium silicofluoride contains both silicon and fluorine, and while as will be discussed hereinafter, a combination of silicating and fluoriding is within the scope of the invention, ammonium silicofluoride probably does not incorporate anything except the fluorine since the silicon is lost during heating. The fluoriding agent can be combined with the alumina in any suitable manner but it is generally done by forming a slurry of the alumina in a solution of the fluoriding agent and a suitable solvent such as alcohol or water. Particularly suitable are one to three carbon atom alcohols because of their volatility and low surface tension. A suitable amount of the solution is utilized to provide the desired concentration of fluorine in the composite after drying. Drying can be effected in a conventional manner, such as suction filtration followed by evaporation or drying under vacuum. In view of the use of a relatively volatile solvent such as methanol, relatively mild conditions such as  $100^\circ\text{C}$  or less can be utilized.

A combination of fluoriding and silicating to give  $\text{F-Si/Al}_2\text{O}_3$  can also be utilized. In such instances, it is preferred to add the fluoriding agent first and most preferred to dry after adding the fluoriding agent before adding the silicating agent. This is because in some instances adding the fluoriding agent after the silicating agent and/or after the chromium can cause an undesirable precipitate. It is possible, however, to add the ingredients in any order.

If desired, the fluorided alumina, silicated alumina or fluorided and silicated alumina can be further treated with a phosphating or phosphiting agent to give a system containing up to five components on adding chromium, i.e.  $\text{P-F-Si-Cr/Al}_2\text{O}_3$ . Thus the phosphated or phosphited support can be  $\text{P-F-Si/Al}_2\text{O}_3$ , or  $\text{P-F/Al}_2\text{O}_3$ . Generally when a phosphating or phosphiting agent is to be used in conjunction with the fluoriding or silicating, the phosphorus treatment is carried out first.

The phosphating or phosphiting agent may be incorporated in an organic water-miscible liquid such as an alcohol and used to treat either a hydrogel or a xerogel. If the starting material is a hydrogel, then the organic liquid/phosphating agent composition effects both the conversion of the hydrogel to a xerogel and provides the phosphating or phosphiting level desired. More specifically if a hydrogel is used, the hydrogel may be washed with water, then with an organic liquid such as isoamyl alcohol or methanol containing the phosphating or phosphiting agent such as phosphoric acid, or phosphorous acid then filtered and the solvent allowed to evaporate. Alternatively the alumina gel can be treated with a vapor of the phosphating or phosphiting agent.

The phosphating or phosphiting agent is preferably used in an amount to react with the alumina to give a P/Al atom ratio of the reaction product on the surface of 0.01:1 to 0.3:1, preferably 0.05:1 to 0.2:1. In practice, however, it is possible to use as much phosphating or phosphiting agent as desired with the excess simply being washed off after the phosphating or phosphiting treatment is complete. The phosphating or phosphiting treatment is generally carried out on alumina which has been previously calcined in air at  $300^\circ\text{C}$ - $700^\circ\text{C}$ . The phosphating or phosphiting treatment is generally carried out at a temperature of  $15^\circ\text{C}$  to  $500^\circ\text{C}$ , preferably room temperature to the boiling point of the solvent if a phosphate or phosphite solution is used or about  $200^\circ\text{C}$  if a vapor is used and a time of 1 minute to 2 hours, preferably 2 minutes to 30 minutes. Generally a methanolic solution of  $\text{H}_3\text{PO}_4$  is used.

Stated in other terms, the phosphorus component is added in an amount to give 1 to 30, preferably 5 to 20 mole percent of the phosphorus compound incorporated based on the total moles of aluminium.

Generally, the ratio of atoms of phosphorus per atom of chromium will be in the range of 100-3000, preferably 500 to 2000. Based on the surface area the phosphorus compound from the phosphating agent is preferably present in an amount sufficient to give about 0.005 to 1, preferably about 0.01 to 0.5 mg P/m<sup>2</sup> of alumina surface as measured by BET nitrogen sorption.

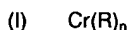
The chromium compound can be any compound in or convertible to the hexavalent state and can be introduced anytime prior to activation. The catalyst contains chromium in an amount generally within the range of about 0.001 to 10, preferably 0.1 to 5, more preferably about 1 weight percent based on the weight of the dried treated alumina support, or since the amount of incorporated treating agent is relatively small, 0.001 to 10, preferably 0.1 to 5, more preferably about 1 weight percent based on the alumina. The chromium compound can be incorporated as known in the art. For instance, a hydrocarbon solution of a material such as tertiary butyl chromate can be used to impregnate the xerogel or an aqueous solution of a chromium compound such as CrO<sub>3</sub> (chromium trioxide), chromium acetate or chromium nitrate can be added to the hydrogel before drying or chromium can be coprecipitated along with the alumina. Preferably the chromium is added after any fluoride treatment and after any phosphorus treatment.

The activation of the chromium-containing catalyst can be carried out at a lower temperature than is generally required for activating silica-based chromium catalysts. Temperatures of 300-900 °C, preferably 500-800 °C, are suitable. The activating ambient can be any oxidizing ambient but for reasons of convenience is generally air. Times of 1 minute to 48 hours, preferably 0.5 to 10 hours are suitable. If desired, the alumina can also be precalcined prior to treatment using the same conditions used later for activation.

In this invention so far as the type of chromium is concerned, an organochromium compound wherein the chromium has less than its maximum valence can be used. The organochromium compounds can include zerovalent compounds such as pi bonded chromium complexes such as dicumene chromium or dibenzene chromium. These pi bonded zerovalent chromium compounds are disclosed in more detail in Delap, U.S. 3,976,632 which issued August 24, 1976. Also suitable are divalent organochromium compounds such as chromocene, bis-(cyclopentadienyl)chromium (II), and substituted derivatives thereof in which the cyclopentadienyl rings contain one or more substituents.

Chromocene offers the advantage of giving high density, ultra high molecular weight polymer. The organochromium compounds on the treated alumina also tend to have exceptional sensitivity to the effects of hydrogen, thus allowing great leeway in the control of molecular weights since the catalyst inherently gives ultra high molecular weight and yet with the sensitivity to hydrogen it is possible to produce polymers with a broad spectrum of molecular weights with a single catalyst.

The currently preferred organochromium compounds, however, are those of either the formula (I) or (II) below:



wherein n is 3 or 4; x is 3 or more; R is -CH<sub>2</sub>MR'R''R'''; wherein M is a Group IVA element, i.e. C, Si, Ge, Sn or Pb; and wherein in a given compound the R groups are identical and R', R'', and R''' are the same or different (preferably the same) hydrocarbyl groups selected from aliphatic and aromatic radicals containing up to about 10 carbon atoms per radical, preferably alkyl radicals containing up to 4 carbon atoms per radical. Also included are combination radicals such as alkaryl. The preferred compound of Formula I is the one wherein M is Si, R', R'' and R''' are methyl (-CH<sub>3</sub>), and n is 4, Cr[-CH<sub>2</sub>Si(CH<sub>3</sub>)<sub>3</sub>]<sub>4</sub>, i.e. tetrakis-(trimethylsilylmethyl)chromium (IV). For Formula II, the preferred compound is the one wherein M is Si, R', R'', and R''' are methyl(-CH<sub>3</sub>), and x=2; i.e. the tetramer, Cr<sub>4</sub>[-CH<sub>2</sub>Si(CH<sub>3</sub>)<sub>3</sub>]<sub>8</sub>, octakis-(μ-trimethylsilylmethyl)tetrachromium(II)

Examples of other suitable compounds of Formula (II) include octakis(benzylidimethylsilylmethyl)tetrachromium and octakis(allyldimethylsilylmethyl)tetrachromium. These compounds on alumina treated in accordance with this invention exhibit activity which is truly remarkable and also exhibit substantial responsiveness to the effects of hydrogen.

It is also possible to use a mixture of two or more chromium components, for instance, as follows: chromium (+6)-chromium (0); chromium (+6)-chromium (+2); chromium (+2)-chromium (0); or two different chromium (0) components or two different chromium (+2) components or a chromium (0) component and a chromium (+2) component. Use of two components selected from chromium (0) and chromium (+2) is particularly desirable.

It is also possible to use mixtures of the total catalyst, i.e. a catalyst of this invention in combination with conventional chromium or vanadium on silica or chromium or vanadium on aluminum phosphate or a titanium or zirconium system.

The amount of organochromium compound relative to the support can range from about 0.02 mmole of chromium compound per gm of support to about 5 mmoles chromium compound per gram support.

The hexavalent Cr catalysts of this invention are generally used in conjunction with a cocatalyst. Suitable cocatalysts include organoaluminum and organoboron compounds. The most preferred boron compounds are trihydrocarbyl boron compounds, particularly tri-n-butylborane, tripropylborane, and triethylborane (TEB). Other suitable boron compounds include trialkyl boron compounds broadly, particularly those having alkyl groups of 1 to 12 carbon atoms, preferably 2 to 5 carbon atoms, triaryl boron compounds such as triphenylborane, alkyl boron alkoxides such as  $B(C_2H_5)_2OC_2H_5$  and halogenated alkyl boron compounds such as  $BC_2H_5Cl_2$ . Suitable aluminum alkyls include  $R_3^I Al$ ,  $R_2^I AlX$  and  $R^I AlX_2$  compounds where  $R^I$  is a 1 to 12 carbon atom hydrocarbyl radical and X is a halogen, preferably chlorine. Triethylaluminum and diethylaluminum chloride are particularly suitable.

The cocatalyst is used in an amount within the range of about 0.2 to 25, preferably 0.2 to 10 parts per million based on the solvent or diluent in systems employing a solvent or diluent. If no solvent or diluent is used the cocatalyst is impregnated onto the catalyst in an amount to give a mole ratio of cocatalyst:chromium (atoms) within the range of 0.5:1 to 5:1. Based on the chromium in the catalyst in systems employing a solvent or diluent the cocatalyst is used in an amount so as to give from 0.01 to 3, preferably 0.1 to 2 times as much boron or aluminum by weight as chromium by weight. Based on atoms of boron or aluminum per atom of chromium, the amount of cocatalyst used will give about 0.05 to about 14, preferably about 0.5 to about 10 atoms of boron or aluminum per atom of chromium.

The cocatalyst can be either premixed with the catalyst or introduced into the reactor as a separate stream, the latter being the preferred procedure.

Of course, the final catalyst can be used with, or contain, other ingredients which do not adversely affect its performance, as, for example, other cocatalysts, antistatic aids in the polymerization zone and other conventional ingredients.

The catalyst of this invention can be used to polymerize at least one mono-1-olefin containing 2 to 8 carbon atoms per molecule, preferably ethylene, propylene, 1-butene, 1-pentene, 1-hexene and 1-octene. The invention is of particular applicability in producing ethylene homopolymers and copolymers from mixtures of ethylene and 0.5 to 20 mole percent of one or more comonomers selected from 1-olefins containing 3 to 8 carbon atoms per molecule. Exemplary comonomers include aliphatic 1-olefins, such as propylene, 1-butene, 1-pentene, 1-hexene, 1-octene and other higher olefins and conjugated or non-conjugated diolefins such as 1,3-butadiene, isoprene, piperylene, 2,3-dimethyl-1,3-butadiene, 1,4-pentadiene, 1,7-hexadiene, and other such diolefins and mixtures thereof. Ethylene copolymers preferably constitute at least about 90, preferably 97 to 99.6 weight percent polymerized ethylene units. Propylene, 1-butene, 1-pentene and 1-hexene are especially preferred comonomers for use with ethylene.

The polymers can be prepared from the catalyst of this invention by solution polymerization, slurry polymerization, and gas phase polymerization techniques using conventional equipment and contacting processes. Contacting of the monomer or monomers with the catalyst can be effected by any manner known in the art of solid catalysts. One convenient method is to suspend the catalyst in the organic medium and to agitate the mixture to maintain the catalyst in suspension throughout the polymerization process. Other known contacting methods such as fluidized bed, gravitating bed, and fixed bed can also be employed. The catalyst of this invention can be used to produce ethylene polymers in a particle form process as disclosed in U.S. 3,624,063 which issued November 30, 1971 to Witt.

The catalyst of this invention is particularly suitable for use in slurry polymerizations. The slurry process is generally carried out in an inert diluent (medium) such as a paraffin, cycloparaffin or aromatic hydrocarbon. For predominantly ethylene polymers, a temperature of about 66-110°C is employed. Pressures in the particle form process can vary from about 110 to about 700 psia (0.76-4.8 MPa) or higher. The catalyst is kept in suspension and is contacted with the monomer or monomers at sufficient pressure to maintain the medium and at least a portion of the monomer or monomers in the liquid phase. The medium and temperature are thus selected such that the polymer is produced as solid particles and is recovered in that form. Generally in slurry polymerization of ethylene homopolymer or predominantly ethylene copolymer systems, the feasible temperature range is 150-230°F (66-110°C).

In polymerizations using a catalyst according to the second aspect of this invention, the chromium compound and the support can be added separately to the reactor. Alternatively, in some instances, particularly in large, continuously run reactors, it may be desirable to briefly premix support and chromium compound in inert diluent such as n-hexane and charge the mixture intermittently as required to sustain the

polymerization reaction at the desired rate.

Catalyst (chromium compound + support) concentrations can be such that the catalyst content ranges from 0.001 to about 1 weight percent based on the weight of the reactor contents.

When hydrogen is used in the prior art, it is generally used at pressures up to 120 psia (0.8 MPa), preferably within the range of 20 to 70 psia (0.14 to 0.48 MPa). Similar amounts can be used in accordance with this invention although smaller amounts are sometimes preferred with the organochromium because of the sensitivity of this catalyst system to the effects of hydrogen. Stated in terms of mole percent hydrogen based on moles of diluent the hydrogen concentration can be from about 0.1 to 10, preferably about 0.2 to 1.25 mole percent, most preferably about 1 mole percent.

Supports employed in the Examples include for the control runs Davison 952 silica and  $\text{AlPO}_4$  made according to U.S. 4,364,841. For the invention runs Davison HPV (high pore volume of about 2.7 mL/g (B.E.T.))  $\text{Al}_2\text{O}_3$  and Ketjen B  $\text{Al}_2\text{O}_3$  were used.

Melt viscosity data are obtained by means of a Rheometrics Dynamic Spectrometer at 230°C using parallel plate geometry. Strain amplitude is 5 percent, nitrogen is used in the sample chamber and the oscillatory frequency is varied from 0.1 to 500 radians/second. The data obtained give storage modulus and loss modulus as a function of oscillatory frequency. From these data in turn can be calculated dynamic complex viscosity  $|\eta^*|$  as described in Chapter 1 of the "Viscoelastic Properties of Polymers", by Ferry, published in 1961 by Wiley. The values obtained are directly related to polymer molecular weight, with the higher the value the higher the molecular weight. It has been shown for a commercially available ultra high molecular weight polyethylene (UHMWPE) that  $|\eta^*|$  when determined at 0.1 radian/second and 190°C has a value of about 30 MPoise.

High load melt index (HLMI) was determined in accordance with ASTM D 1238, condition 7.

#### Example 1

##### Fluorided Alumina-Hexavalent Cr Catalysts and Ethylene Polymerization

A series of catalysts containing combined fluorine and high pore volume alumina was prepared by impregnating the alumina with a methanolic solution of  $\text{Cr}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  sufficient to provide a calculated 1.5 weight percent Cr based on the dry catalyst, drying the mixture and impregnating same with a methanolic solution of  $\text{NH}_4\text{HF}_2$  sufficient to give the specified amount of combined fluorine as weight percent based on the dry catalyst. Each catalyst was activated for polymerization by calcining in dry air at the specified time and temperature.

Ethylene was polymerized in a 2 l stirred stainless steel reactor containing 1.25 lbs (567 g) of isobutane with portions of each catalyst and with 8 ppm TEB (1 ml TEB, 0.5 weight percent in n-hexane) as cocatalyst at 85°C. The pressure (3.9 MPa) was maintained by supplying ethylene as needed from a pressurized reservoir.

The conditions used and results obtained are set forth in Table I.

**TABLE I**  
Ethylene Polymerization With Cr<sup>+6</sup>-Fluorided Al<sub>2</sub>O<sub>3</sub>  
Catalyst and TEB Cocatalyst, 565 PSIA (3.9 MPa) Total Pressure

Run No.	Calculated Wt. % F	Calcining		Reaction Temp. °C	Reaction Time, Min.	Calculated Productivity g/30 min.	Polymer	
		Temp. °C	Hours				Yield g	MLMI g/10 min.
Control	0	700	3	96	60	250	46	-
1	1.7	700	3	85	30	1230	110	0
2	2.0	700	3	85	32	950(1013) <sup>(a)</sup>	85	0
3	2.3	600	3	85	30	1365	105	0
4	2.7	700	1	85	25	2730(1820) <sup>(a)</sup>	137	0
5	3.4	600	3	85	30	Trace	-	-

(a) Normalized to 30 minute run time assuming a linear relationship over the time period. The values in the brackets are calculated productivity for the actual run times.

The results for invention runs 1-4, of Table I all show that fluoriding alumina gives more active catalysts based on productivity results compared to the results obtained in the control run. That is, productivity is increased from about 3.8 to 8.7-fold by the fluoriding treatment, with the catalyst containing about 2.7

weight percent combined fluorine being the most active. Ultra high molecular weight polymer, having a melt viscosity of 40 to 50 was obtained.

Run 1 further shows that very small amounts of F are effective Run 5 shows that above 3 weight percent F there is a dramatic deterioration in catalyst activity. Depending on other factors such as surface area, it is believed that 5 percent is the most that would possibly be beneficial, with 3 percent generally being the upper limit.

#### Example 2

##### 10 Silicated, Fluorided Alumina-Hexavalent Cr Catalysts And Ethylene Polymerization

A series of catalysts containing combined fluorine, silica and high pore volume alumina was prepared by impregnating the alumina with Silbond 40® as the silica source,  $(\text{NH}_4)_2\text{SiF}_6$  or  $\text{NH}_4\text{HF}_2$  as the fluoride source and  $\text{Cr}(\text{C}_2\text{H}_3\text{O}_2)_3 \cdot \text{H}_2\text{O}$  or  $\text{Cr}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  as the Cr source in the manner described before. Each mixture was then dried and activated (calcined) for polymerization by heating in dry air for the specified time.

Ethylene was polymerized, as before, with portions of each catalyst and with 8.3 ppm TEB or TEA (triethylaluminum, one instance) as cocatalyst, and in one run, in the presence of 5 cc (ml) of 1-hexene and hydrogen.



The conditions used and results obtained are presented in Table II.

**TABLE II**  
Ethylene Polymerization With Cr<sup>+6</sup>-Silicated, Fluorided Al<sub>2</sub>O<sub>3</sub>  
Catalyst, TEB Or TEA Cocatalyst, 565 PSIA (3.9 MPa) Total Pressure

Run No.	Calculated, Wt. %		Temp., °C		Run Time min.	Calc. Prod. g/30/min.	Yield g		Polymer	
	SiO <sub>2</sub>	F	Act.	Reaction					HLMI	Melt visc. MPoise
1(a)	0	0	2.0	700	96	250	46	-	(b)	-
2	1.0	1.8	1.5	600	85	945	135	0	0	43
3	1.3	2.6	1.5	600	85	2000	140	0	0	54
4(c)	1.3	2.6	1.5	600	100	900(750)(f)	35	0.8	0.8	-
5(d)	1.6	3.2	1.5	600	85	120(80)	8	-	-	-
6(e)	2.5	2.0	2.0	700	85	2410	170	0	0	55
7	4.0	2.2	1.5	700	85	1440	105	0	0	39
8	4.0	2.2	1.5	750	85	1300	98	0	0	-
9	2.5	2.7	1.5	700	85	1015	150	0	0	-
10	3.2	2.2	4.0	700	85	2100	160	0	0	-
11	4.8	2.2	1.5	700	85	2380	129	0	0	-

(a) Same as the control run, Table I.

(b) A dash signifies no determination was made.

(c) Run made with 5.0 cc (mL) 1-hexene and 50 psi (345 kPa) H<sub>2</sub>. The calculated productivity is normalized to 30 minutes run time as in previous tables. The value in brackets is 750 g/25 minutes run time.

(d) Calculated productivity is normalized to 30 minutes run time. The value in brackets is 80 g/20 minutes run time.

(e) Used 8.3 ppm TEA as cocatalyst. All other runs made with 8.3 ppm TEB as cocatalyst.

(f) Apparently the catalyst was accidentally deactivated.

Inspection of the results set forth in Table II shows that the invention catalysts in runs 2-11 are active in polymerizing ethylene to very high molecular weight homopolymers in the absence of hydrogen based on the zero HLMI results. The melt viscosity values of 43, 54, 55 and 39 megapoise shown in runs 2, 3, 6, and

7 are considered to be indicative of ultrahigh molecular weight polyethylene. The catalyst is also rather insensitive to hydrogen as shown in run 4 since the HLMI of the ethylene/1-hexene copolymer made is 0.8. This value is indicative of a high molecular weight polymer. The low productivity of 120 g polymer per g catalyst per 30 minutes is believed to be an anomalous result. The catalyst was apparently deactivated, perhaps inadvertently contacting a poison during its production or in the polymerization process.

### Example 3

#### Production Of Ethylene Polymers In Scaled-Up Runs With Silicated, Fluorided Alumina-Hexavalent Chromium Catalyst Alone and in Admixture With Hexavalent Chromium-Aluminum Phosphate Catalyst

Several silicated, fluorided high pore volume alumina-hexavalent Cr catalysts were prepared in the manner outlined before. In one instance, the alumina was treated with Silbond 40® and  $\text{Cr}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  in the presence of isopropanol and the mixture dried overnight in a vacuum oven at 80 °C. The next day the solid product was mixed with  $\text{NH}_4\text{HF}_2$  and methanol and that product dried in a vacuum oven as before. The dry product was activated (calcined) in dry air for 3 hours at 700 °C to give invention catalyst L.

In the second instance, all the catalytic components employed in invention catalyst L were mixed together in the presence of methanol, dried in a vacuum oven and calcined as above to form invention catalyst M.

Each catalyst, on a dry basis (calcined) was calculated to contain about 4 weight percent silica, about 2.1 weight percent each of chromium and fluorine, the balance-being alumina.

A portion of each catalyst was mixed with another conventional catalyst consisting of 1 weight percent hexavalent chromium on aluminum phosphate, P/Al atom ratio of 0.9, the catalyst being activated for 3 hours at 700 °C in dry air. This catalyst is called O, for convenience.

Ethylene alone and in some instances ethylene admixed with 1-hexene was polymerized in a 23 gal (87 liter) loop reactor in a continuous process at the specified temperatures employing isobutane as diluent, triethylborane (TEB) as cocatalyst and the indicated amount of hydrogen as adjuvant. In this process, catalyst was intermittently charged as a slurry in n-hexane at a rate sufficient to maintain the desired production of polymer. The product in slurry form was intermittently removed from the reactor through a settling leg, flashed to remove diluent and volatile gases and stored. The resulting "fluff" was stabilized with a conventional multicomponent system sufficient to provide about a total of 0.2 weight percent stabilizers, e.g. 2,6-di-t-butyl-4-methylphenol, dilauryl thiodipropionate, zinc stearate, prior to evaluating it for various physical properties.

The catalyst systems, reaction conditions and results obtained are set forth in Table III and IIIA.

TABLE III

## Ethylene Polymerization, Single Catalyst, No Hydrogen

Run No.	Cat No.	TEB ppm	Calculated Productivity g/g cat/hr.	Reactor Temp., °C	Polymer		
					Density, g/cc (g/ml)	Intrinsic Visc. dl/g	Melt Viscosity MPoise
					Fluff (a)	Molded	
1	L	1	1330	93	0.474	0.9402	16
2	L	2	1590	93	0.468	0.9401	15
3	H	3	2500	93	0.450	0.9412	14
4	H	1	1320	83	0.474	0.9414	-
5	H	4	1650	82	0.482	0.9402	16.5
6	H	4	1740	82	0.461	0.9403	insoluble
7	H	4	1920	87	0.471	0.9400	insoluble
8	H	4	2040	88	0.460	0.9408	insoluble
9	H	4	1450	88	0.455	0.9398	11.6

(a) Bulk density.

(b) A dash signifies no determination made.

TABLE III-A  
Ethylene Polymerization, Mixed Catalyst, With Hydrogen

Run No.	Mixed Catalyst Component		Calculated Prod., g/g/hr	H <sub>2</sub> Mole %	1-Hexene Wt %	TEB ppm	Reactor Temp. °C	Polymer		Flex Mod. MPa	ESCR Cont. A
	L, wt %	O, wt %						Density, g/cc	Pellet ILMH		
10	79	21	1450	1.00	0	0.51	97	0.404	0.9580	6.7	1450 >1000
11	79	21	1280	1.23	0	0.79	99	0.420	0.9586	16	1450 >1000
12	79	21	1750	0.85	0	1.03	99	0.428	0.9594	23	1410 >1000
13	79	21	1850	0.50	0	1.01	99	0.415	0.9590	14	1430 >1000
14	79	21	1610	0.33	1.6	1.06	99	0.426	0.9577	20	1390 >1000
15	67	33	1750	0.16	3.6	1.12	93	0.439	0.9551	42.5	1280 >1000
16	67	33	1640	0.09	3.5	1.08	91	0.431	0.9540	23	1190 >1000
17	67	33	2170	0.13	2.9	1.06	86	0.392	0.9561	15	1260 >1000

(a) ASTM D-790.

(b) Bulk density.

The results presented in Table III show in runs 1-3, at a constant reactor temperature that productivity increases with increasing TEB level, bulk density decreases, molded density remains about the same and polymer molecular weight is decreasing based on intrinsic viscosity data. Although, the intrinsic viscosity results are less than 20, except for runs 6-8 where the polymer was too high molecular weight to dissolve, the melt viscosity results suggest that UHMWPE is made in all the runs, thus all are considered to be

invention runs. At a constant TEB level of 4 ppm the results in runs 5-8 indicate that as reactor temperatures increase, productivity also increases and polymer bulk density decreases although little change in molded density is seen. The productivity results obtained are sufficiently high to be of commercial interest.

5 Table IIIA shows the results of ethylene homopolymers and ethylene/1-hexene copolymers prepared with catalyst mixtures containing the invention catalysts. These bimodal homopolymers prepared in runs 10-13 have a higher density than those listed in Table II, reflecting the influence of the  $\text{AlPO}_4$ -containing catalyst. As TEB level increases in these runs, productivity also increases as before. All polymers show pellet (pelletized fluff) HLMI values ranging from about 7 to 43, and outstanding ESCR for the high stiffness,  
10 indicating that good film could be produced from at least some of them, e.g. those having a HLMI of about 20 or less. As expected, with decreasing density, the flexural moduli of the polymer samples also decrease.

#### Example 4

15 The following data is presented to illustrate what is believed to be an unusual characteristic of polymers made with the  $\text{Cr}(6+)/\text{F-Al}_2\text{O}_3$  catalyst system. As disclosed in the body of this application, this catalyst produces ultrahigh molecular weight polyethylene, UHMWPE. Generally speaking, density is found to decrease with molecular weight in this type of polymer in the prior art. The hexavalent chromium system mentioned above is unusual in that the UHMWPE polymer produced has the highest density yet observed  
20 for polymers of similar molecular weight. Molecular weight is usually correlated to the viscosity of a standardized decalin solution of the polymer according to ASTM procedures D-4020-81, D-2857-70 and D-1601-78. Another, less conventional measure of molecular weight is obtained from the melt viscosity of the polymer using a Rheometrics Dynamic Spectrometer operating at  $230^\circ\text{C}$  and .1 radians per second oscillation frequency. The data in Figures 1 and 2 illustrate the above mentioned relationships. For both  
25 measures of molecular weight, namely melt and intrinsic viscosity, the  $\text{Cr}(6+)/\text{F-Al}_2\text{O}_3$  catalyst is shown to produce polymer with higher densities than any of the numerous control catalysts within a similar range of molecular weights.

Specifically novel polymers are provided having a melt viscosity (M Poise) of 35 or greater, more specifically about 40-60 or in some instances 50 or greater and a density of 0.940 g/cc (g/ml) or greater,  
30 more specifically about 0.940 to 0.950 (g/ml), preferably greater than 0.945 g/cc (g/ml). Based on intrinsic viscosity, novel polymers are provided having an intrinsic viscosity of greater than 13 g/dL, more specifically 13 to 17 g/dL or in some instances 15 to 20 g/dL at a density of greater than 0.940 (g/ml), more specifically at a density of 0.940 to 0.950 (g/ml), more preferably at a density at greater than 0.941 g/cc (g/ml).

35

#### Claims

1. A method of producing a fluorided and, optionally, surface silicated alumina catalyst composition, characterized by contacting alumina with a fluoriding agent to produce a fluorided alumina, said  
40 fluorided alumina containing in addition a chromium component, the resulting composition being activated by heating in an oxygen-containing ambient at a temperature within the range of  $300$  to  $900^\circ\text{C}$  so as to convert at least a portion of the chromium of said chromium component to the hexavalent state and combining the resulting hexavalent chromium-containing catalyst with a cocatalyst.
- 45 2. The method of claim 1, wherein said silicating comprises contacting said alumina with a silicating agent in solution or in vaporous form and thereafter converting said silicating agent to silica on the surface of said alumina.
3. The method of claim 1 or 2, wherein said fluoriding agent is ammonium bifluoride.
- 50 4. The method of claim 3, wherein said ammonium bifluoride is provided in an amount sufficient to give 0.5 to 5 weight percent fluorine on said alumina based on the weight of said alumina.
5. The method of claim 3 or 4, wherein said fluoriding agent is introduced by forming a slurry of said  
55 alumina in a solution of said fluoriding agent.
6. The method of claim 1 or 2, wherein said silicating agent is a polymeric siloxane and said polymeric siloxane after said treating is converted to silica on the surface of said alumina by calcining in air at a

temperature within the range of 500 to 800 °C.

7. The method of claim 1, 2 or 6, wherein said silicating agent is used in an amount sufficient to give 0.5 to 10 weight percent silica based on the weight of the alumina.
8. The method of claim 1, 2, 6 or 7, wherein said contacting with said silicating agent is carried out in a slurry of said alumina in said solution of said silicating agent in a 1 to 6 carbon atom alcohol.
9. The method of any of claims 1, 2 and 6 to 8, wherein said contacting with said silicating agent is carried out in a slurry of said alumina in said solution of said silicating agent after which the composition is dried and thereafter said fluoriding agent is added by forming a slurry of the thus dried composition in a solution of said fluoriding agent.
10. The method of any of claims 1, 2 and 6 to 9, wherein said alumina has been treated with ammonium bifluoride and an alcoholic solution of polymeric siloxane form of tetraethoxysilane.
11. The method of any of the preceding claims, characterized by additionally subjecting said alumina to a phosphating or phosphiting treatment.
12. The method of claim 11, wherein said alumina is calcined in air at 300-700 °C and thereafter contacted with a methanol solution of phosphoric acid prior to contact with said silicating agent or fluoriding agent.
13. The method of claim 1, wherein said activation is carried out at a temperature of from 500 to 800 °C.
14. The method of claim 1, wherein said cocatalyst is selected from organoboron compounds and organoaluminum compounds.
15. The method of claim 14, wherein said cocatalyst is triethylborane.
16. The method of any of the preceding claims, wherein said chromium component is selected from chromium trioxide, chromium acetate and chromium nitrate.
17. The method of any of claims 1 to 15, wherein said chromium component is an organo chromium compound having chromium in a valence less than the maximum valence for chromium.
18. The method of any of the preceding claims, wherein said chromium component is included in an amount sufficient to give 0.1 to 5 weight percent chromium based on the weight of alumina.
19. The method of claim 1, wherein said oxygen-containing ambient is air.
20. The use of the catalyst composition as obtained in any of claims 1 to 19 for the polymerization or copolymerization of mono-1-olefins.

#### Patentansprüche

1. Verfahren zur Herstellung einer fluoridierten und gegebenenfalls an der Oberfläche silicierten Aluminiumoxid-Katalysator-Zusammensetzung, gekennzeichnet durch Kontaktieren von Aluminiumoxid mit einem Fluoridierungsmittel zur Herstellung von fluoridiertem Aluminiumoxid, wobei das fluoridierte Aluminiumoxid zusätzlich eine Chromkomponente enthält, wobei die erhaltene Zusammensetzung durch Erwärmen in einer sauerstoffhaltigen Umgebung auf eine Temperatur im Bereich von 300 bis 900 °C aktiviert wird, so daß mindestens ein Teil des Chroms der Chromkomponente in den sechswertigen Zustand umgewandelt wird, und Mischen des erhaltenen, sechswertiges Chrom enthaltenden Katalysators mit einem Kokatalysator.
2. Verfahren nach Anspruch 1, wobei das Silicieren das Kontaktieren des Aluminiumoxids mit einem Silicierungsmittel in Lösung oder in Gasform und die anschließende Umwandlung des Silicierungsmittels in Siliciumdioxid auf der Oberfläche des Aluminiumoxids umfaßt.

3. Verfahren nach Anspruch 1 oder 2, wobei es sich bei dem Fluoridierungsmittel um Ammoniumbifluorid handelt.
- 5 4. Verfahren nach Anspruch 3, wobei das Ammoniumbifluorid in einer ausreichenden Menge bereitgestellt wird, um 0,5 bis 5 Gew.-% Fluor auf dem Aluminiumoxid, bezogen auf das Gewicht des Aluminiumoxids, zu ergeben.
- 10 5. Verfahren nach Anspruch 3 oder 4, wobei das Fluoridierungsmittel durch Bildung einer Aufschlämmung des Aluminiumoxids in einer Lösung des Fluoridierungsmittels eingeführt wird.
6. Verfahren nach Anspruch 1 oder 2, wobei es sich bei dem Silicatierungsmittel um ein polymeres Siloxan handelt und das polymere Siloxan nach der Behandlung auf der Oberfläche des Aluminiumoxids durch Calcinieren an der Luft bei einer Temperatur im Bereich von 500 bis 800 °C in Siliciumdioxid umgewandelt wird.
- 15 7. Verfahren nach Anspruch 1, 2 oder 6, wobei das Silicatierungsmittel in einer ausreichenden Menge verwendet wird, um 0,5 bis 10 Gew.-% Siliciumdioxid, bezogen auf das Gewicht des Aluminiumoxids, zu ergeben.
- 20 8. Verfahren nach Anspruch 1, 2, 6 oder 7, wobei das Kontaktieren mit dem Silicatierungsmittel in einer Aufschlämmung des Aluminiumoxids in der Lösung des Silicatierungsmittels in einem Alkohol mit 1 bis 6 Kohlenstoffatomen durchgeführt wird.
- 25 9. Verfahren nach einem der Ansprüche 1, 2 und 6 bis 8, wobei das Kontaktieren mit dem Silicatierungsmittel in einer Aufschlämmung des Aluminiumoxids in der Lösung des Silicatierungsmittels durchgeführt wird, wonach die Zusammensetzung getrocknet und anschließend das Fluoridierungsmittel in Form einer Aufschlämmung der so getrockneten Zusammensetzung in einer Lösung des Fluoridierungsmittels eingeführt wird.
- 30 10. Verfahren nach einem der Ansprüche 1, 2 und 6 bis 9, wobei das Aluminiumoxid mit Ammoniumbifluorid und einer alkoholischen Lösung der polymeren Siloxanform von Tetraethoxysilan behandelt worden ist.
- 35 11. Verfahren nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß das Aluminiumoxid zusätzlich einer Phosphatierungs- oder Phosphitierungsbehandlung unterworfen wird.
- 40 12. Verfahren nach Anspruch 11, wobei das Aluminiumoxid an der Luft bei 300-700 °C calciniert und anschließend mit einer methanolischen Lösung von Phosphorsäure in Kontakt gebracht wird, bevor es mit dem Silicatierungsmittel oder dem Fluoridierungsmittel in Kontakt gebracht wird.
13. Verfahren nach Anspruch 1, wobei die Aktivierung bei einer Temperatur von 500 bis 800 °C durchgeführt wird.
- 45 14. Verfahren nach Anspruch 1, wobei der Cokatalysator unter Organoborverbindungen und Organoaluminiumverbindungen ausgewählt ist.
15. Verfahren nach Anspruch 14, wobei es sich bei dem Cokatalysator um Triethylboran handelt.
- 50 16. Verfahren nach einem der vorstehenden Ansprüche, wobei die Chromkomponente unter Chromtrioxid, Chromacetat und Chromnitrat ausgewählt ist.
17. Verfahren nach einem der Ansprüche 1 bis 15, wobei es sich bei der Chromkomponente um eine Organochromverbindung mit Chrom in einer geringeren Wertigkeit als der maximalen Wertigkeit von Chrom handelt.
- 55 18. Verfahren nach einem der vorstehenden Ansprüche, wobei die Chromverbindung in einer ausreichenden Menge einverleibt wird, daß sich 0,1 bis 5 Gew.-% Chrom, bezogen auf das Gewicht des Aluminiumoxids, ergeben.

19. Verfahren nach Anspruch 1, wobei die sauerstoffhaltige Umgebung Luft ist.

20. Verwendung der nach einem der Ansprüche 1 bis 19 erhaltenen Katalysatorzusammensetzung für die Polymerisation oder Copolymerisation von Mono-1-olefinen.

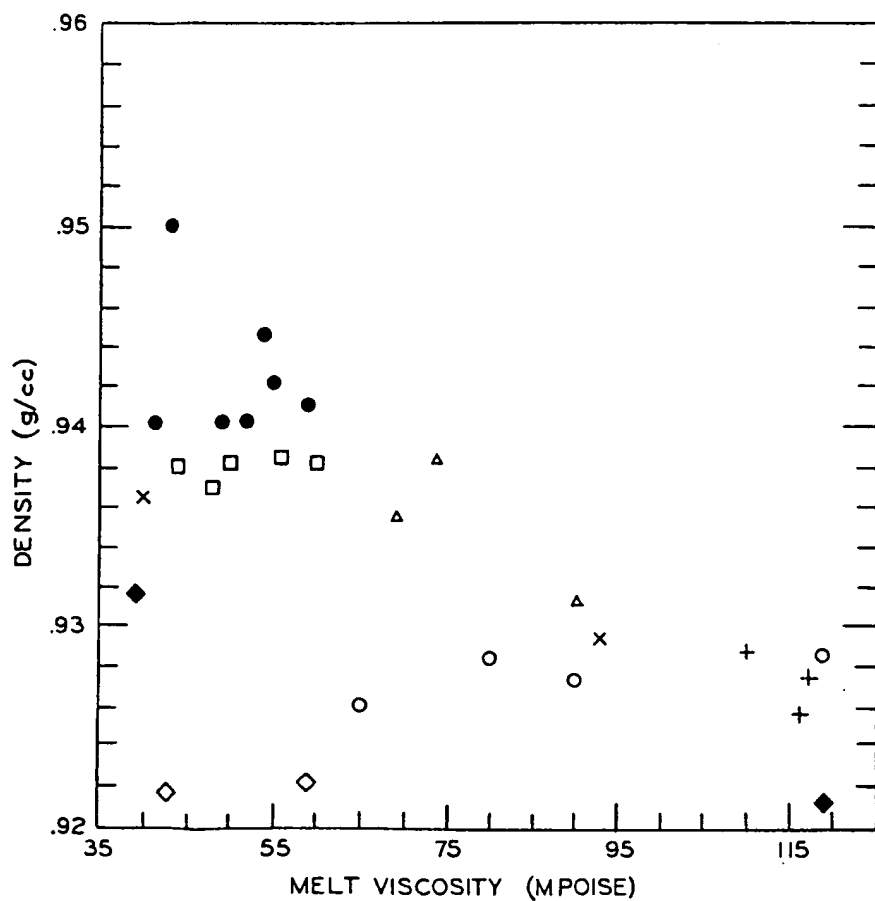
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# Revendications

1. Un procédé pour produire une composition de catalyseur d'alumine fluorée et, éventuellement, silicatée en surface, caractérisé en ce qu'il consiste à mettre en contact de l'alumine avec un agent de fluoration pour produire une alumine fluorée, ladite alumine fluorée renfermant, en outre, un composé de chrome, la composition résultante étant activée par chauffage dans une atmosphère renfermant de l'oxygène à une température comprise dans la gamme de 300 à 900 °C afin de transformer au moins une partie du chrome dudit composé de chrome à l'état hexavalent et à combiner le catalyseur résultant contenant du chrome hexavalent avec un cocatalyseur.
2. Le procédé selon la revendication 1 dans lequel ladite silication consiste à mettre en contact ladite alumine avec un agent de silication en solution ou sous la forme de vapeur et à transformer ensuite ledit agent de silication en silice à la surface de ladite alumine.
3. Le procédé selon la revendication 1 ou la revendication 2 dans lequel ledit agent de fluoration est le bifluorure d'ammonium.
4. Le procédé selon la revendication 3 dans lequel ledit bifluorure d'ammonium est prévu en une quantité suffisante pour avoir 0,5 à 5% en poids de fluor dans l'alumine, calculés sur le poids de ladite alumine.
5. Le procédé selon la revendication 3 ou la revendication 4 dans lequel ledit agent de fluoration est introduit en formant une bouillie de ladite alumine dans une solution dudit agent de fluoration.
6. Le procédé selon la revendication 1 ou la revendication 2 dans lequel ledit agent de silication est un siloxane polymère et ledit siloxane polymère est transformé après ledit traitement en silice à la surface de ladite alumine par calcination dans l'air à une température comprise dans la gamme de 500 à 800 °C.
7. Le procédé selon la revendication 1, 2 ou 6 dans lequel ledit agent de silication est utilisé en une quantité suffisante pour avoir 0,5 à 10% en poids de silice calculés sur le poids de l'alumine.
8. Le procédé selon la revendication 1, 2, 6 ou 7 dans lequel la mise en contact avec ledit agent de silication est réalisée dans une bouillie de ladite alumine dans ladite solution dudit agent de silication dans un alcool comprenant de 1 à 6 atomes de carbone.
9. Le procédé selon l'une quelconque des revendications 1, 2 et 6 à 8 dans lequel ladite mise en contact avec ledit agent de silication est mise en oeuvre dans une bouillie de ladite alumine dans ladite solution dudit agent de silication après quoi la composition est séchée et ensuite ledit agent de fluoration est ajouté en formant une bouillie de la composition ainsi séchée dans une solution dudit agent de fluoration.
10. Le procédé selon l'une quelconque des revendications 1, 2 et 6 à 9 dans lequel ladite alumine a été traitée avec du bifluorure d'ammonium et une solution alcoolique de siloxane polymère de tétraéthoxysilane.
11. Le procédé selon l'une quelconque des revendications précédentes caractérisé en ce qu'il consiste à soumettre, en outre, ladite alumine à un traitement de phosphatation ou de phosphitation.
12. Le procédé selon la revendication 11 dans lequel ladite alumine est calcinée dans l'air à une température de 300 à 700 °C et est ensuite mise en contact avec une solution méthanolique d'acide phosphorique avant la mise en contact avec ledit agent de silication ou ledit agent de fluoration.



13. Le procédé selon la revendication 1 dans lequel ladite activation est mise en oeuvre à une température d'environ 500 à 800 °C.
14. Le procédé selon la revendication 1 dans lequel ledit cocatalyseur est choisi parmi les composés de bore organiques et les composés d'aluminium organiques.
15. Le procédé selon la revendication 14 dans lequel ledit cocatalyseur est le triéthylborane.
16. Le procédé selon l'une quelconque des revendications précédentes dans lequel ledit composé de chrome est choisi parmi le trioxyde de chrome, l'acétate de chrome et le nitrate de chrome.
17. Le procédé selon l'une quelconque des revendications 1 à 15 dans lequel ledit composé de chrome est un composé de chrome organique ayant du chrome à une valence inférieure à la valence maximale pour le chrome.
18. Le procédé selon l'une quelconque des revendications précédentes dans lequel ledit composé de chrome est incorporé en une quantité suffisante pour avoir de 0,1 à 5% en poids de chrome calculés sur le poids d'alumine.
19. Le procédé selon la revendication 1 dans lequel ladite atmosphère renfermant de l'oxygène est de l'air.
20. L'utilisation de la composition de catalyseur comme obtenue dans l'une quelconque des revendications 1 à 19 pour la polymérisation ou la copolymérisation de mono-1-oléfines.



- Cr(6+)/F-Al<sub>2</sub>O<sub>3</sub> CATALYST
- TiCl<sub>4</sub>/SiO<sub>2</sub>-TEA
- △ TETRABENZYLZIRCONIUM/AlPO<sub>4</sub>
- VC12/P-Al<sub>2</sub>O<sub>3</sub>-TEA
- ◆ CHROMOCENE/AlPO<sub>4</sub>
- ◇ CHROMOCENE + Cr(2+)/AlPO<sub>4</sub>
- + CHROMOCENE/F-Al<sub>2</sub>O<sub>3</sub>
- x COMMERCIAL UHMWPE RESIN, GUR 413, FROM HOECHST

FIG. 1

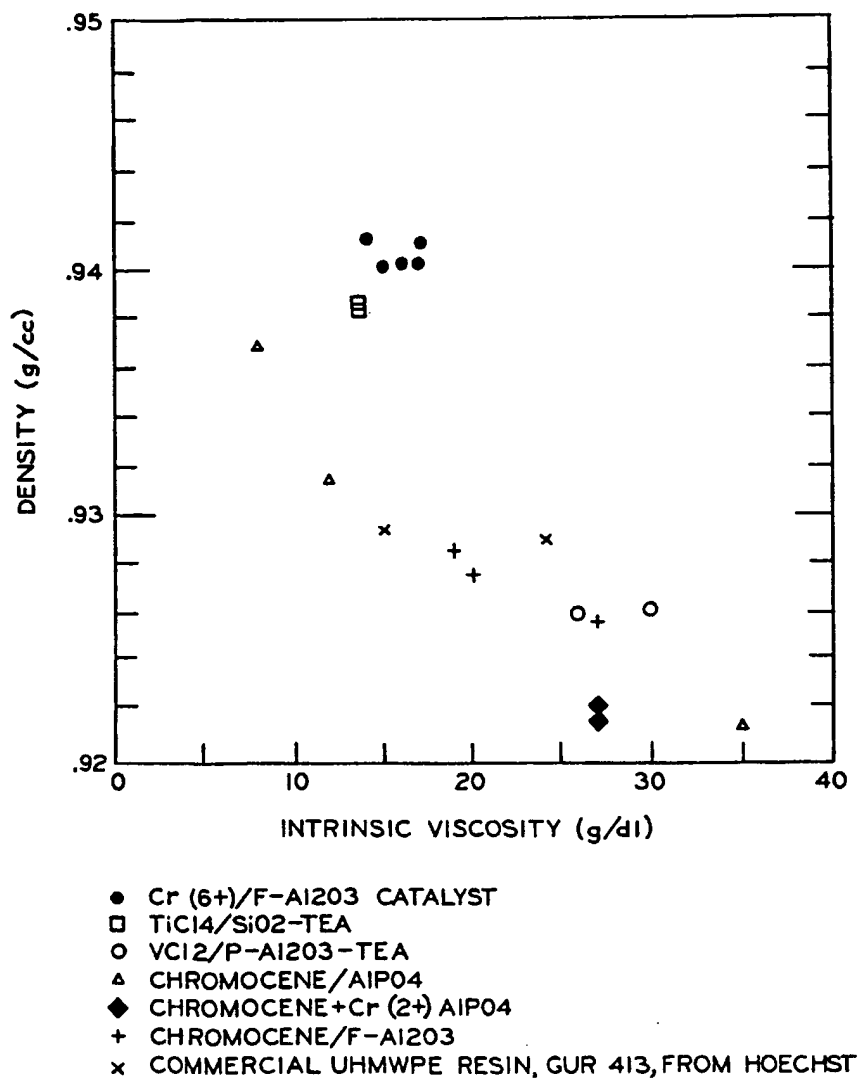


FIG. 2